

# PCI BIG BEAM COMPETITION

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CENE 486 - FINAL PRESENTATION



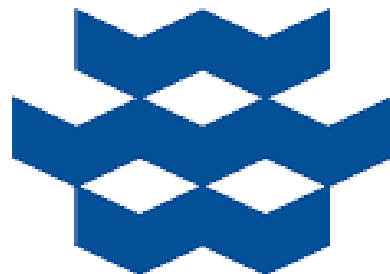
# STAKEHOLDERS



Figure 1. NAU Logo



Figure 2. PCI Logo



Architectural and Structural Precast Concrete  
An **EnCon** Company

Figure 3. TPAC Logo

# PROJECT INTRODUCTION

## Purpose:

- Analyze, design, and test a prestressed concrete beam

## Technical Aspects and Considerations:

- Rules for the competition
  - 20-foot long beam
  - Crack after 20 kips
  - Break between 32-40 kips

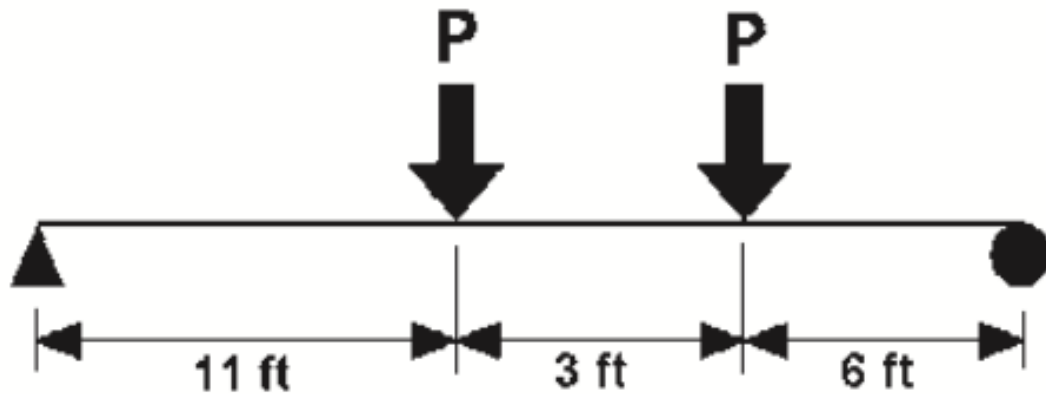


Figure 4. Load Distribution

# MILESTONES

- Task 1: Preliminary Research
- Task 2: Preliminary Beam Design
- Task 3: Final Design and Analysis
- Task 4: Predictions
- Task 5: Shop Drawings
- Task 6: Casting of Beam
- Task 7: Testing of Beam
- Task 8: Project Management
- Task 9: Project Impacts

# TASK 1: PRELIMINARY RESEARCH

## 1.1 Three Stages of Design Prestressed Concrete Beam

- Release
- Cracking load
- Ultimate strength

## 1.2 Preliminary Cross-Section Designs

- I-beam
- T-beam
- Box
- Hollow Box

## 1.3 Preliminary Decision Matrix

- Determine decision matrix criteria based off PCI scoring

# TASK 1.1: THREE STAGES OF DESIGN PRESTRESSED CONCRETE BEAM

- Release (1)

$$\sigma_{tp} := \frac{P}{A} + \frac{M_{PS} \cdot c}{I}$$

- Cracking load (2)

$$\sigma_{crack} := 7.5 \sqrt{f_{c28}} = \frac{P}{A} + \frac{M_{PS} \cdot c}{I} + \frac{M_D \cdot c}{I} + \frac{M_{LL} \cdot c}{I}$$

- Ultimate strength (3)

$$m := A_p \cdot f_p \left( d - \frac{\beta_1 \cdot c}{2} \right) + M_{LL}$$

P = Vertical Load

A = Area

$M_{PS}$  = Moment prestress

c = Distance from fiber to neutral axis

I = Moment of Inertia

$f_{c28}$  = 28 compressive stress

$M_D$  = Moment dead load

$M_{LL}$  = Moment live load

$A_p$  = Area Prestressing

$f_p$  = Stress due to prestress

$\beta_1$  = Depth factor

# TASK 1.1: THREE STAGES OF DESIGN PRESTRESSED CONCRETE BEAM

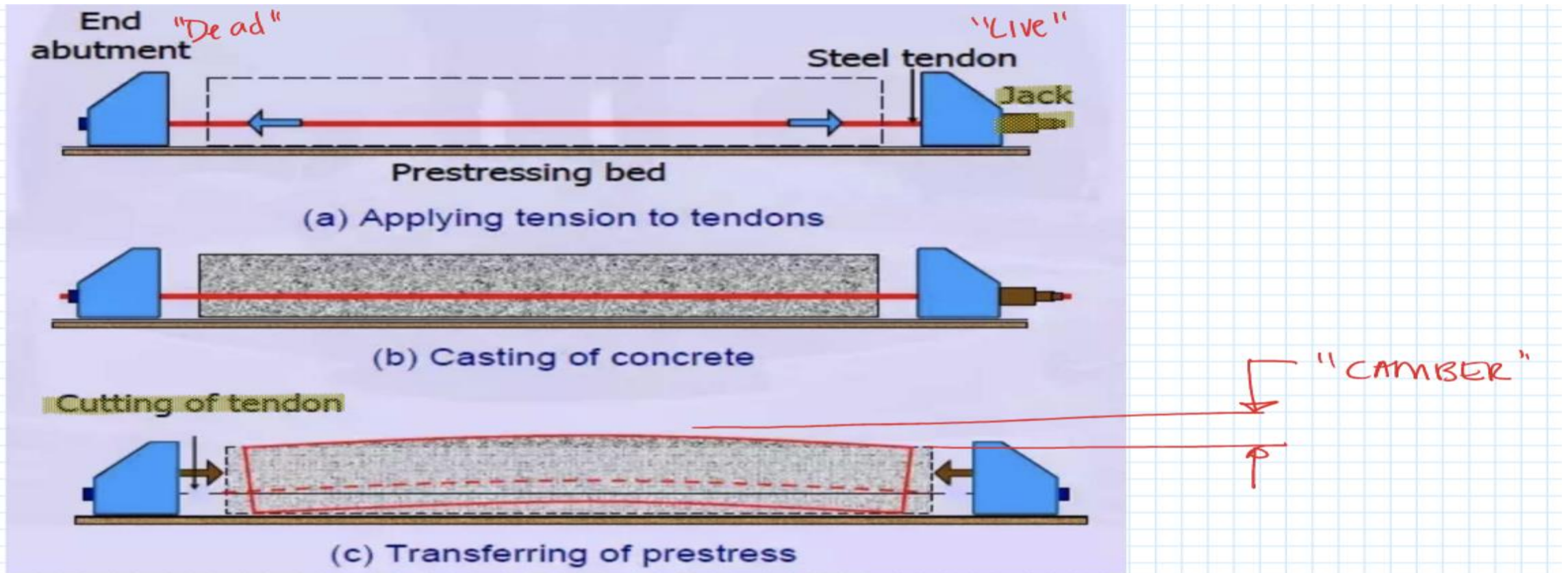


Figure 5. Release Process

# TASK 1.2: PRELIMINARY DESIGNS

I-Beam

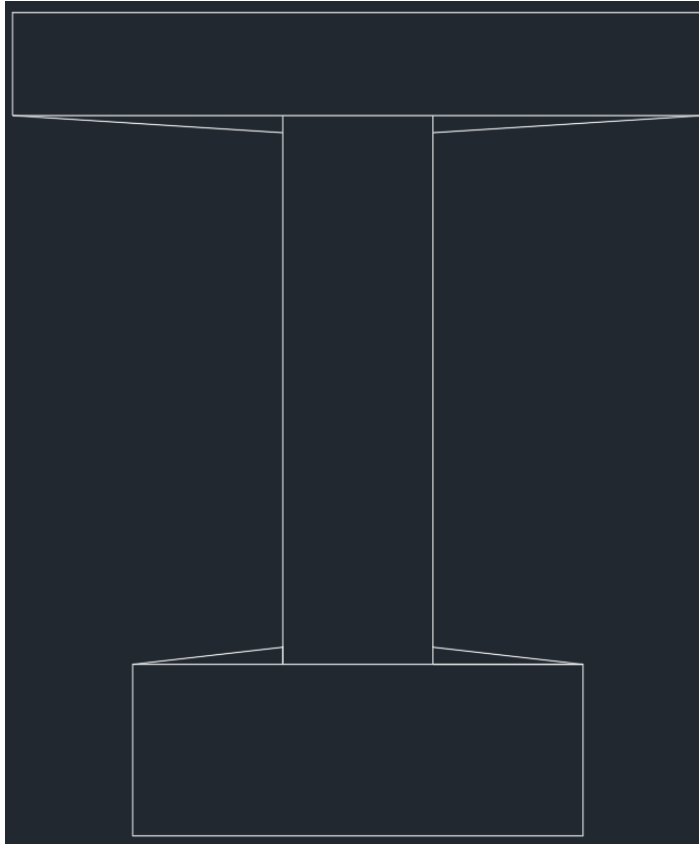


Figure 6. I-Beam

T-Beam

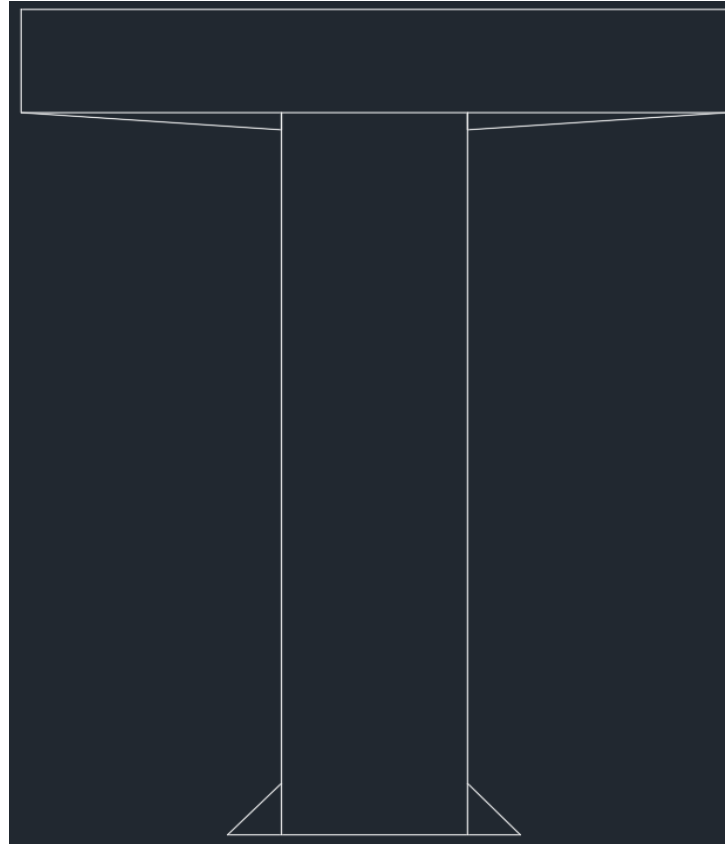


Figure 7. T-Beam

Box

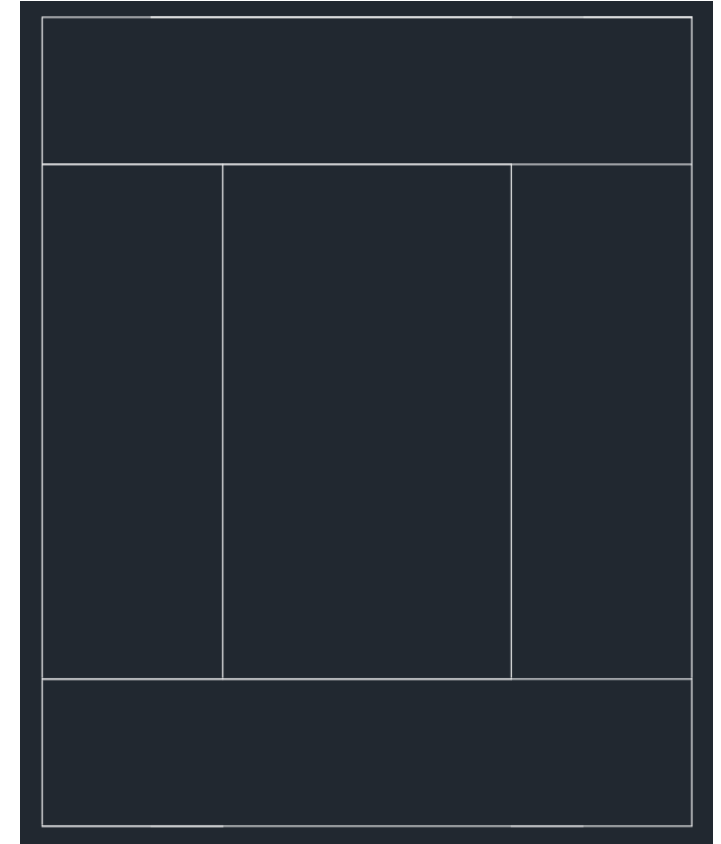


Figure 8. Hollow Box



# TASK 1.3: PRELIMINARY DECISION MATRIX

- Determine decision matrix criteria based off PCI scoring
  - Lowest cost
  - Lowest weight
  - Largest deflection



Figure 9. PCI Logo

# TASK 2: PRELIMINARY BEAM DESIGN

## 2.1 Initial Beam Designs

- Design 6 beam options with different depths and cross sections

## 2.2 Final Decision Matrix

- Mix selection
- Beam selection



Figure 10. MathCAD Logo

# TASK 2.1: INITIAL BEAM DESIGN

- Design 6 beam options with different depths and cross sections

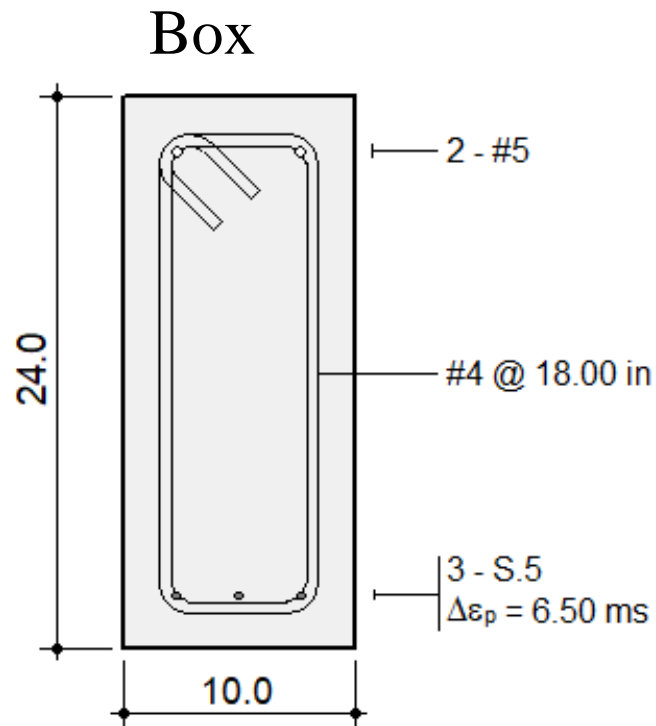


Figure 11. Box

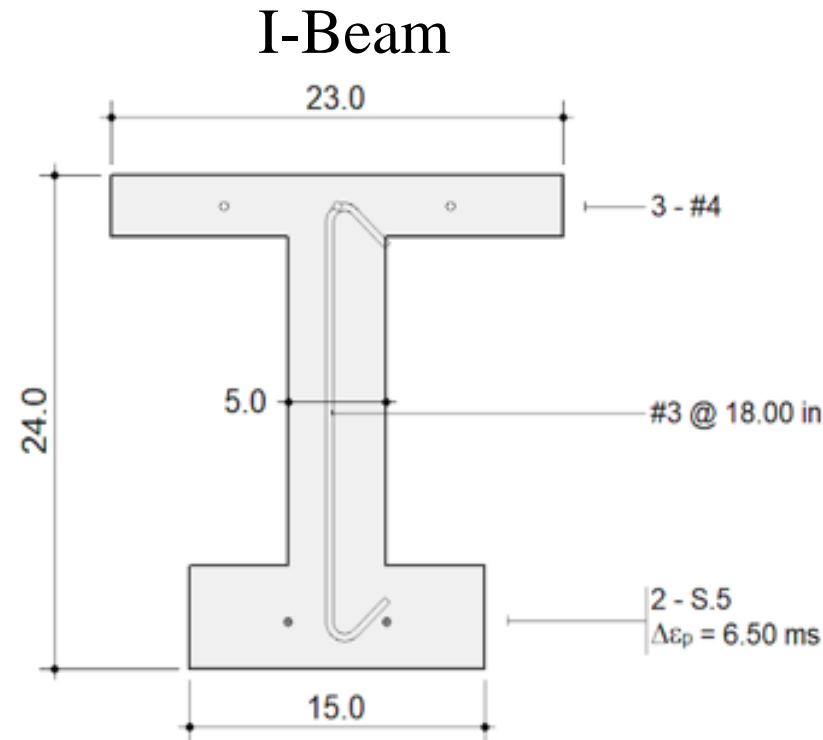


Figure 12. I-Beam

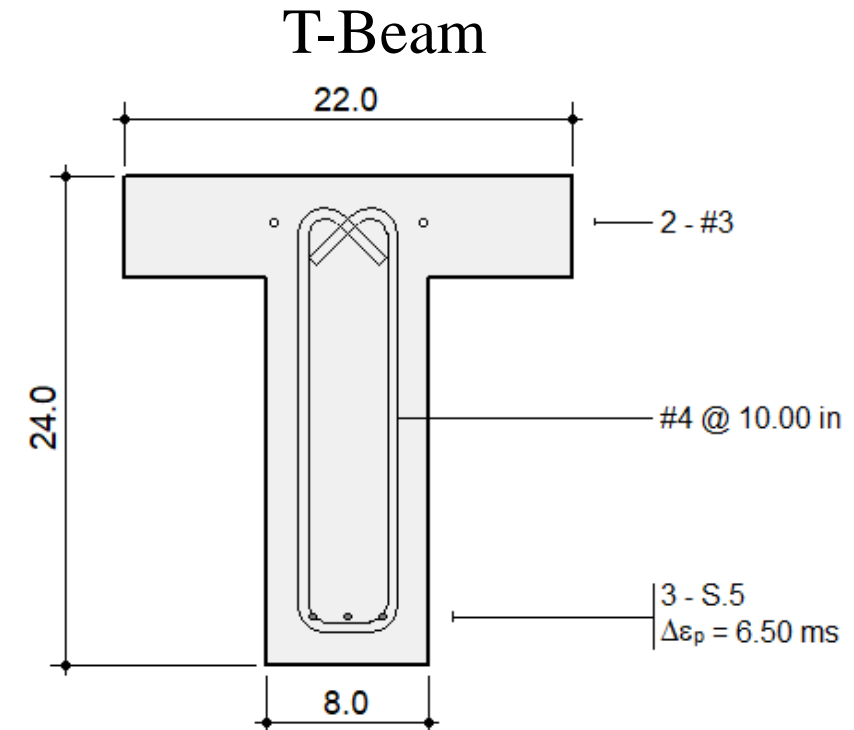


Figure 13. T-Beam

## TASK 2.2: DECISION MATRIX

| Beam Decision Matrix |               |              |                             |              |                     |             |              |
|----------------------|---------------|--------------|-----------------------------|--------------|---------------------|-------------|--------------|
| <i>Cross Section</i> | Cost (\$)     | Score        | <i>Weight of Beam (pcf)</i> | Score        | Deflection (inches) | Score       | Total Score  |
| T Beam LW            | 218.52        | 1.48         | 6069.18                     | 5.17         | 7.04                | 10.00       | 16.65        |
| T Beam NW            | 218.52        | 1.48         | 7277.99                     | 0.91         | 7.25                | 5.96        | 8.35         |
| <b>I Beam LW</b>     | <b>183.13</b> | <b>10.00</b> | <b>4697.05</b>              | <b>10.00</b> | <b>7.25</b>         | <b>6.09</b> | <b>26.09</b> |
| I Beam NW            | 183.13        | 10.00        | 5632.58                     | 6.71         | 7.46                | 1.97        | 18.68        |
| Hollow Box Beam LW   | 224.66        | 0.00         | 6285.22                     | 4.41         | 7.35                | 4.06        | 8.47         |
| Hollow Box Beam NW   | 224.66        | 0.00         | 7537.07                     | 0.00         | 7.57                | 0.00        | 0.00         |

Table 1. Beam Decision Matrix

# TASK 3: PRELIMINARY RESEARCH

**3.1 Shear Design**

**3.2 Reinforcement Design**

**3.3 Cracking Load**

**3.4 Max Load at Midspan**



Figure 14. Bending Beam

# TASK 3.1: SHEAR DESIGN

$$V_{cia} := .6\lambda \cdot \sqrt{f_c} \cdot b_w \cdot d_p + v_d + \frac{v_i \cdot M_{cre}}{M_{max}}$$

$$V_{cib} := 1.7\lambda \cdot \sqrt{f_c} \cdot b_w \cdot d_p$$

$$V_{cw} := (3.5\lambda \cdot \sqrt{f_c} + .3f_{pc}) \cdot b_w \cdot d_p + v_p$$

Figure 15. Equations for Shear

$V_{cia}$  = Flexure Shear Capacity

$\lambda$  = factor for density of concrete

$f_c$  = Compressive stress of concrete

$b_w$  = base width

$d_p$  = distance from compression steel to prestressing

$v_d$  = shear force due to dead load

$v_i$  = shear force due to max moment

$M_{cre}$  = Moment of cracking due to applied load

$M_{max}$  = Maximum moment

$V_{cib}$  = Flexure Shear Capacity

$V_{cw}$  = Web Shear Capacity

$f_{pc}$  = Compressive stress of concrete resisting external loads

$v_p$  = Vertical effective prestress force

## TASK 3.1: SHEAR DESIGN

- Shear design is based off the smaller value of the Flexure Shear Capacity ( $V_{ci}$ ) and Web Shear Capacity ( $V_{cw}$ )
- Calculated at the support that has maximum shear and the load point which has the maximum shear
- No.3 stirrups at 18" spacing were used on beam

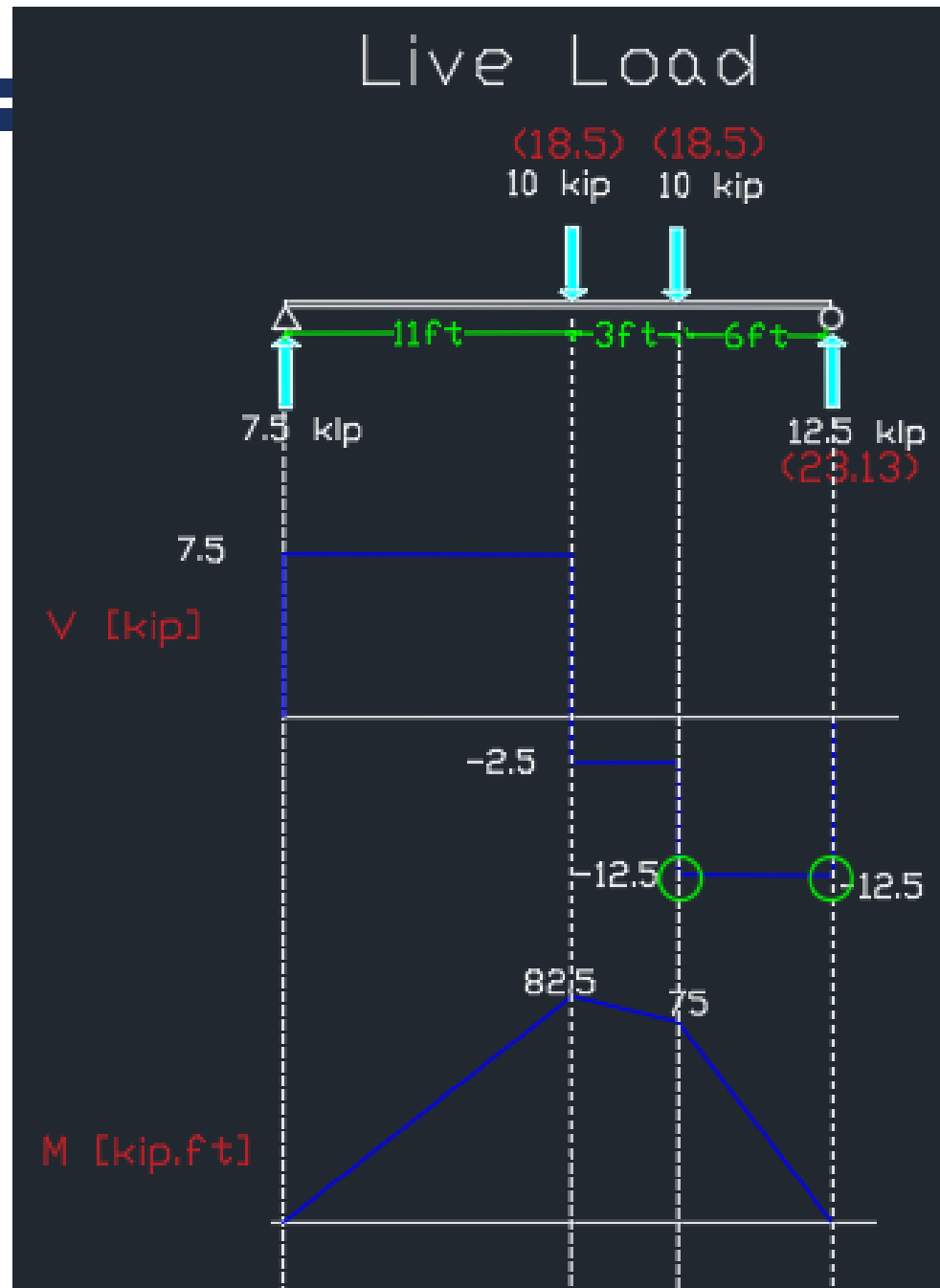


Figure 16. Live Load Diagrams



# Self Weight

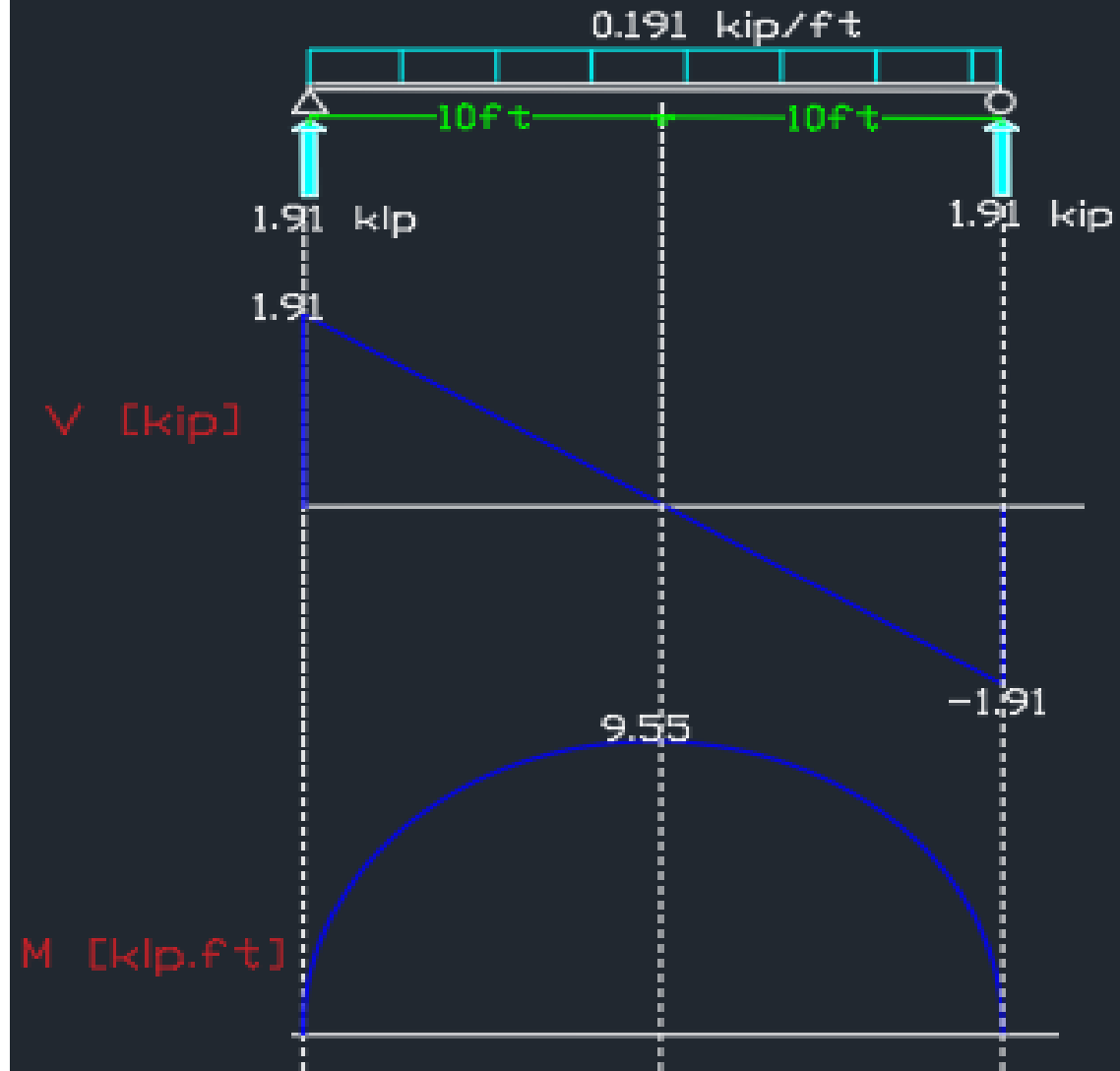


Figure 17. Self Weight Diagram

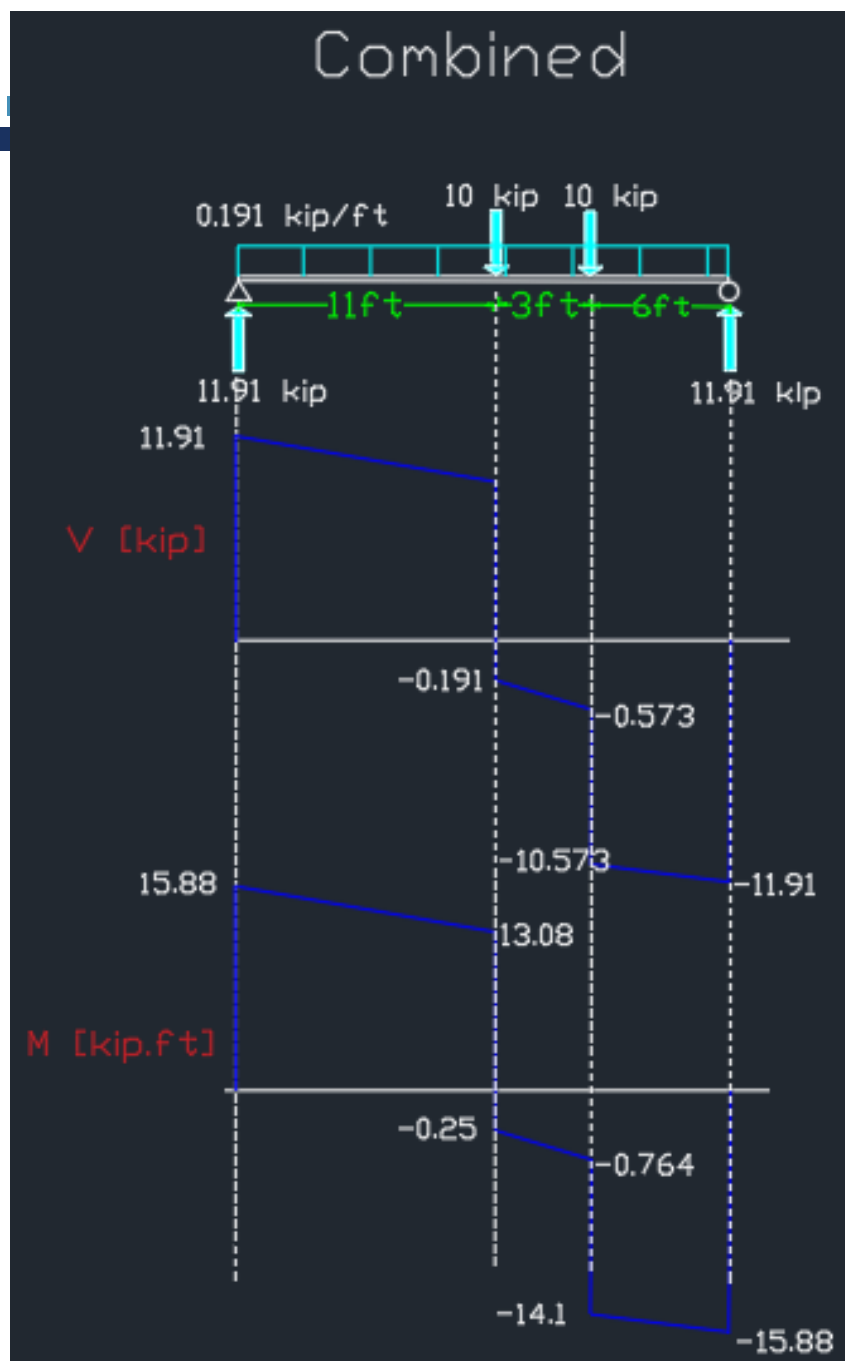


Figure 18. Combined Diagram

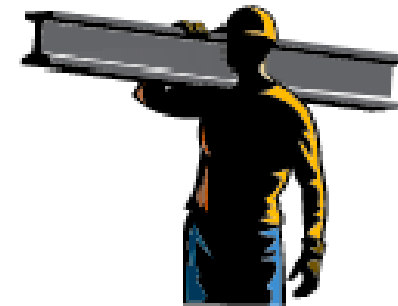
# TASK 3.2: REINFORCEMENT DESIGN

Compression Steel (top of beam)

- 3 No. 4 bars

Prestressing Strand (bottom of beam)

- 2 of .5” Diameter Low Relax Strands



## The Big Beam Theory

Figure 19. Big Beam Theory Logo

# TASK 3.3: CRACKING LOAD

## Cracking Capacity:

$$\omega_{sw} := (A_{gconcrete} \cdot \gamma_c) = 191.163 \cdot \frac{\text{lbf}}{\text{ft}}$$

$$L := 20\text{ft}$$

$$M_{sw} := \frac{(\omega_{sw} \cdot L^2)}{8} = 9.558 \cdot \text{ft} \cdot \text{kip}$$

$$\sigma_{sw} := M_{sw} \cdot \frac{y_{bar28}}{I_{tr28}} = 83.755 \cdot \text{psi}$$

$$f_{cr} := 7.5\text{psi} \sqrt{\frac{f_{c28}}{\text{psi}}} = 670.82 \cdot \text{psi}$$

$$MLL := 1\text{kip} \cdot \text{in}$$

Given

$$f_{cr} = \left[ -\sigma_a + \sigma_{sw} - \sigma_f + \frac{(MLL \cdot y_{bar28})}{I_{tr28}} \right]$$

$$MLL := \text{Minerr}(MLL)$$

$$P_{cr} := \frac{2 \cdot (MLL)}{8\text{ft}} = 21.083 \cdot \text{kip}$$

$$MLL = 84.332 \cdot \text{kip} \cdot \text{ft}$$

21.083 kip

Figure 20. MathCAD Sheet for Cracking Load

# TASK 3.4: MAX LOAD AT MIDSPAN

## Ultimate Capacity

$$d := y_1 = 22.5 \cdot \text{in}$$

$$d_{\text{prime}} := y_6 = 2.5 \cdot \text{in}$$

$$\beta := \begin{cases} 0.85 & \text{if } (f_{c28} \leq 4000 \text{psi}) \\ \left[ 0.85 - \left[ 0.5 \cdot \left( \frac{f_{c28} - 4000 \text{psi}}{1000 \text{psi}} \right) \right] \right] & \text{if } 4000 \text{psi} < f_{c28} < 8000 \text{psi} \\ 0.65 & \text{if } f_{c28} \geq 8000 \text{psi} \end{cases} = 0.65$$

Initial Guess:  $\underline{c} := 1 \text{in}$       Strain in Concrete at Failure:  $\underline{\epsilon} := .003$

Given

$$(0.85 \cdot f_{c28} \cdot \beta \cdot c \cdot b_1) + \min \left[ A_{s\text{prime}} \cdot \epsilon \cdot \left[ \frac{(c - d_{\text{prime}})}{c} \right] \cdot E_s, f_y \cdot A_{s\text{prime}} \right] - A_p \cdot f_u = 0$$

$$\underline{c} := \text{Minerr}(c) = 1.284 \cdot \text{in} \quad h_3 = 5 \cdot \text{in}$$

$$\text{Check in Flange} := \begin{cases} \text{"Okay"} & \text{if } c \leq h_3 \\ \text{"Incorrect Assumption"} & \text{if } c > h_3 \end{cases}$$

Check in Flange = "Okay"

$$C_c := 0.85 f_{c28} \beta \cdot c \cdot b_1 = 130.528 \cdot \text{kip} \quad \epsilon = 3 \times 10^{-3}$$

$$C_s := A_{s\text{prime}} \cdot E_s \cdot \epsilon \cdot \left[ \frac{(c - y_6)}{c} \right] = -49.438 \cdot \text{kip}$$

$$\underline{T} := A_p \cdot f_u = 81.09 \cdot \text{kip}$$

$$M_n := f_u \cdot A_p \cdot [d - (\beta \cdot c \cdot 0.5)] + C_s \cdot (\beta \cdot c \cdot 0.5 - d_{\text{prime}}) = 157.804 \cdot \text{ft} \cdot \text{kip}$$

$$P_n := \frac{[(M_n - M_{sw}) \cdot 2]}{8 \text{ft}} = 37.062 \cdot \text{kip}$$

37.062 kip

Figure 21. MathCAD Sheet for Max Load

# TASK 4: PREDICTIONS

## 4.1 Response 2000

- Moment curvature and Internal moment and axial force

## 4.2 Prediction Calculations

- Deflection
- Camber



Response  
2000

Figure 22. Response 2000 Logo

| Geometric Properties       |             |                |
|----------------------------|-------------|----------------|
|                            | Gross Conc. | Trans (n=6.34) |
| Area (in <sup>2</sup> )    | 224.0       | 228.8          |
| Inertia (in <sup>4</sup> ) | 16332.9     | 16818.2        |
| $y_t$ (in)                 | 11.6        | 11.5           |
| $y_b$ (in)                 | 12.4        | 12.5           |
| $S_t$ (in <sup>3</sup> )   | 1409.3      | 1480.1         |
| $S_b$ (in <sup>3</sup> )   | 1316.0      | 1347.5         |

**Full Member Properties**

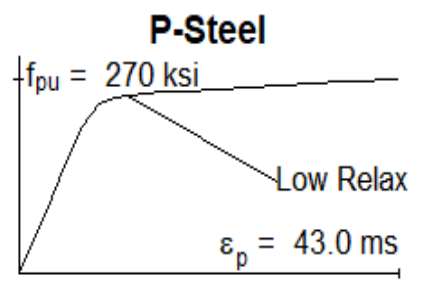
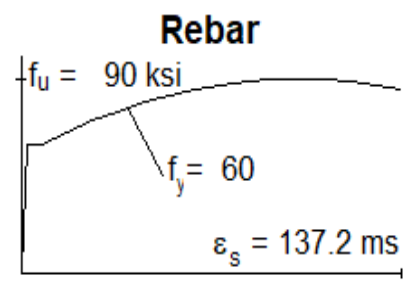
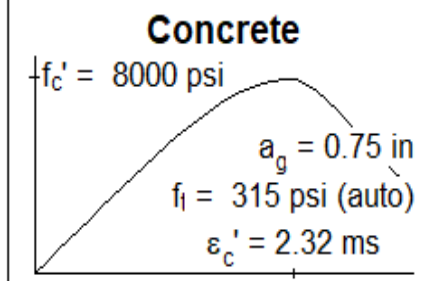
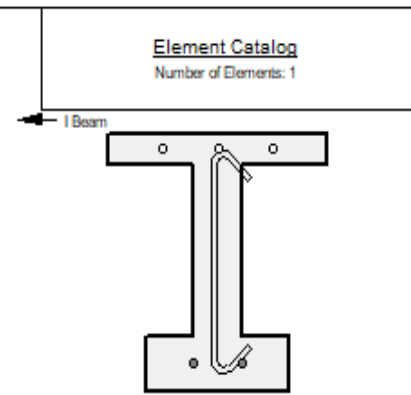
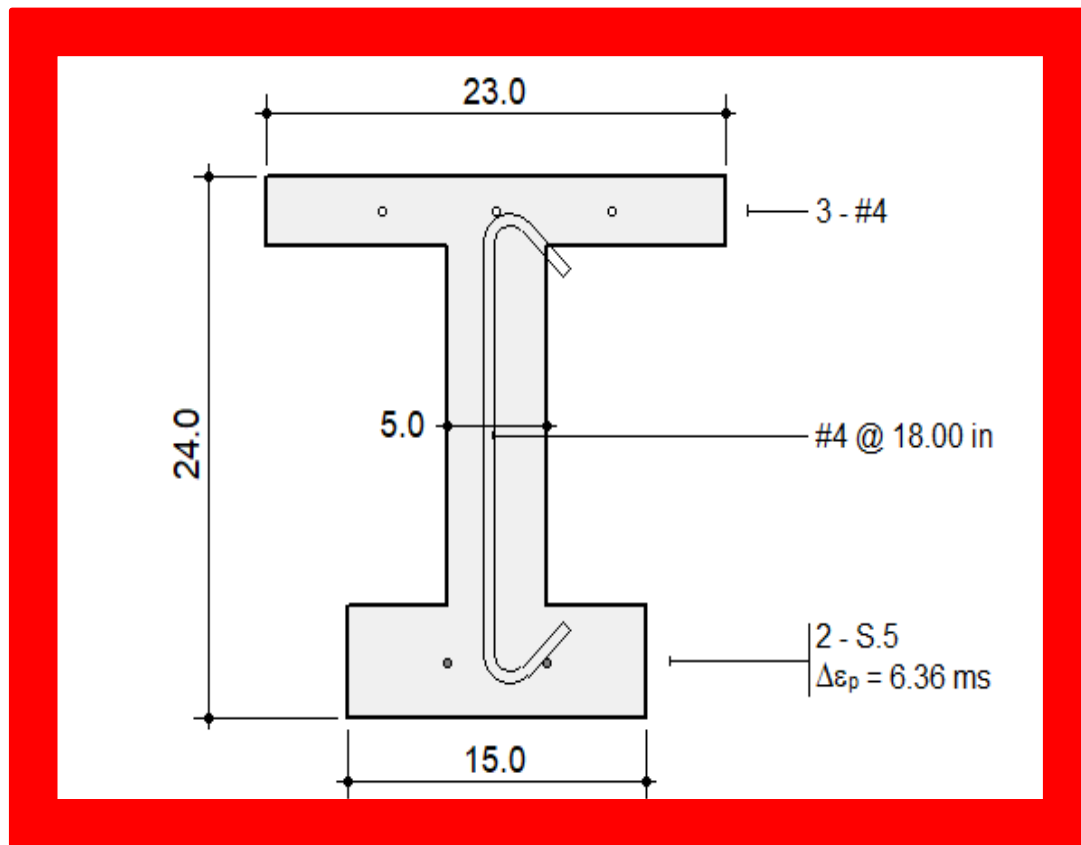
Length: 104.0 in with perfect anchorage  
 Roller @ 8.0 in ( $\theta=0, \Delta_y \neq 0$ ) @ 104.0 in  
 3 Definitions for live load moment diagram

**Crack Spacing**

2 x dist + 0.1  $d_b$  / p

**Loading (N, M, V + dN, dM, dV)**

0.0, 0.0, 0.0 + 0.0, 0.738, 0.0



All dimensions in inches  
 Clear cover to reinforcement = 1.25 in



**I Beam**

**The Big Beam Theory**

Figure 23. Response 2000 Input

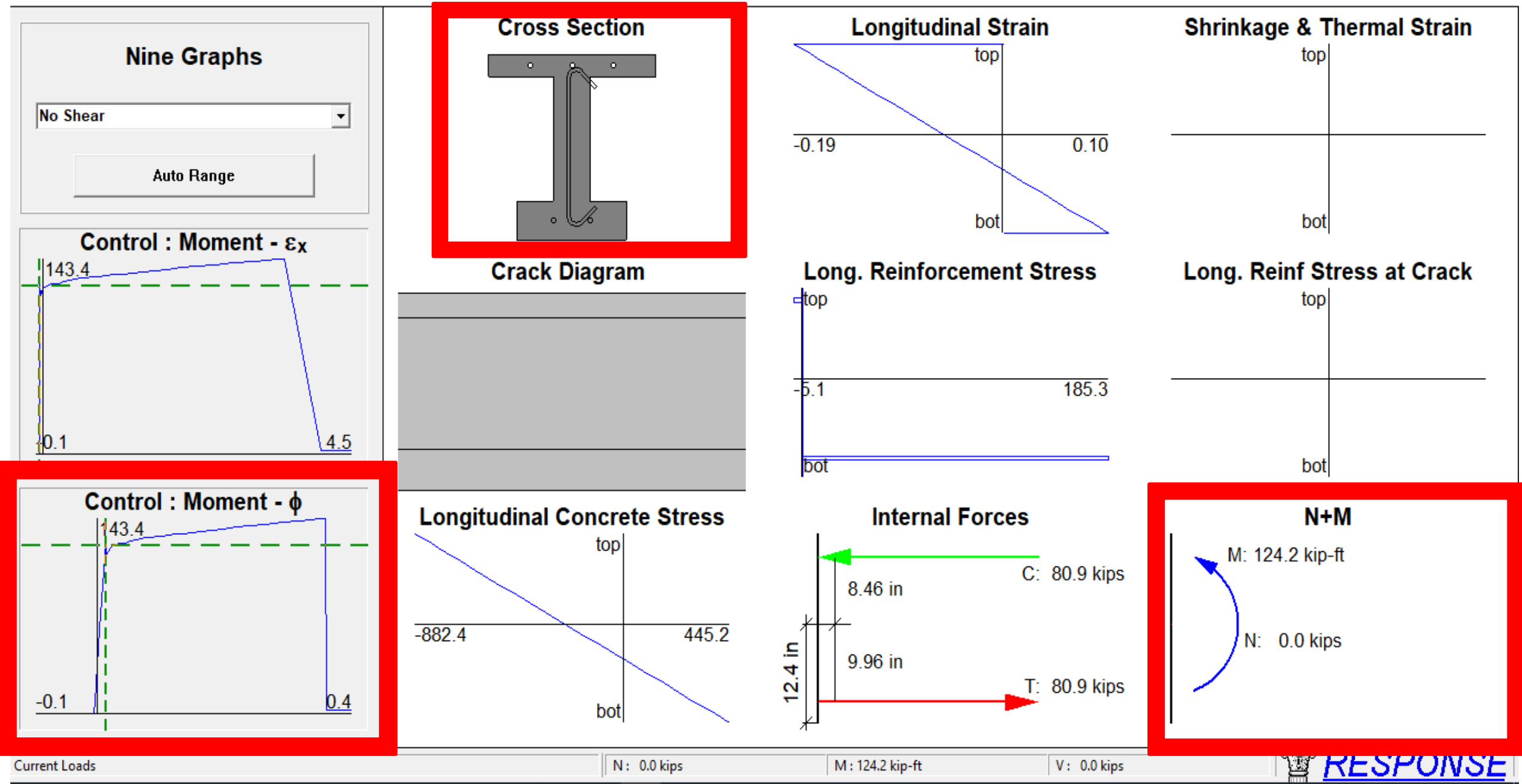


Figure 24. Response 2000 Output



# TASK 4.1: RESPONSE 2000

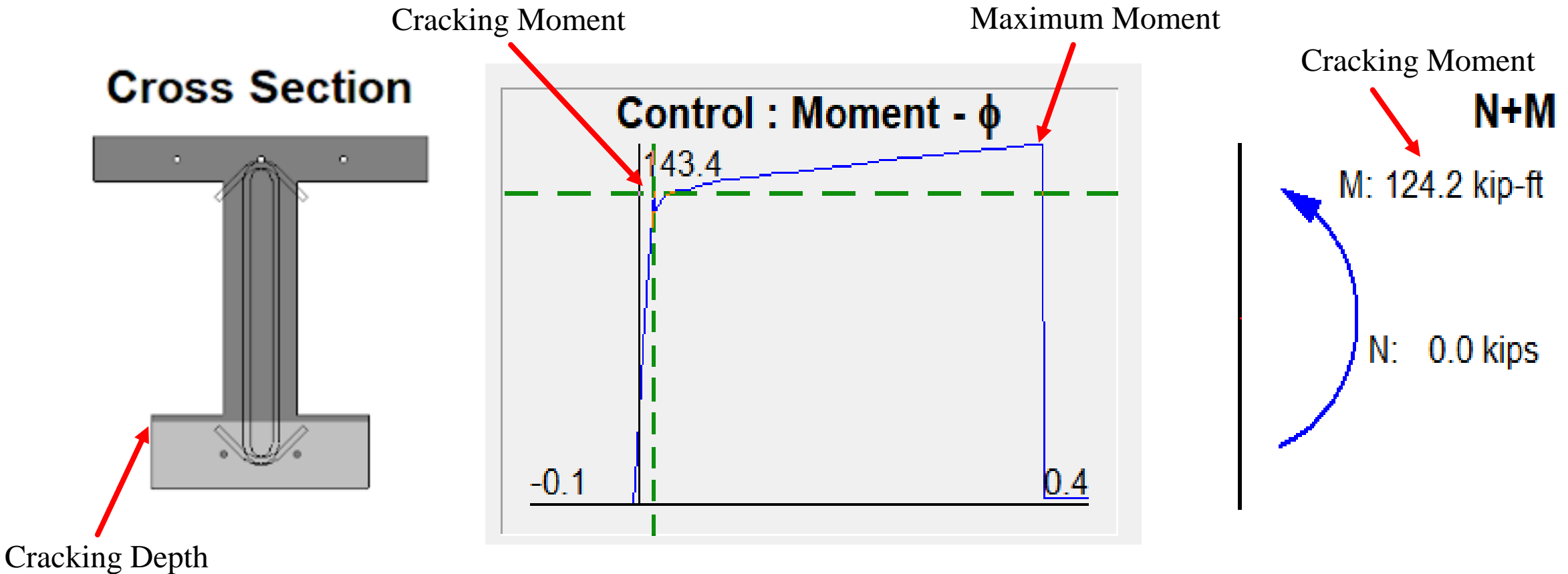


Figure 25. Response 2000 Output

# TASK 4.1: RESPONSE 2000

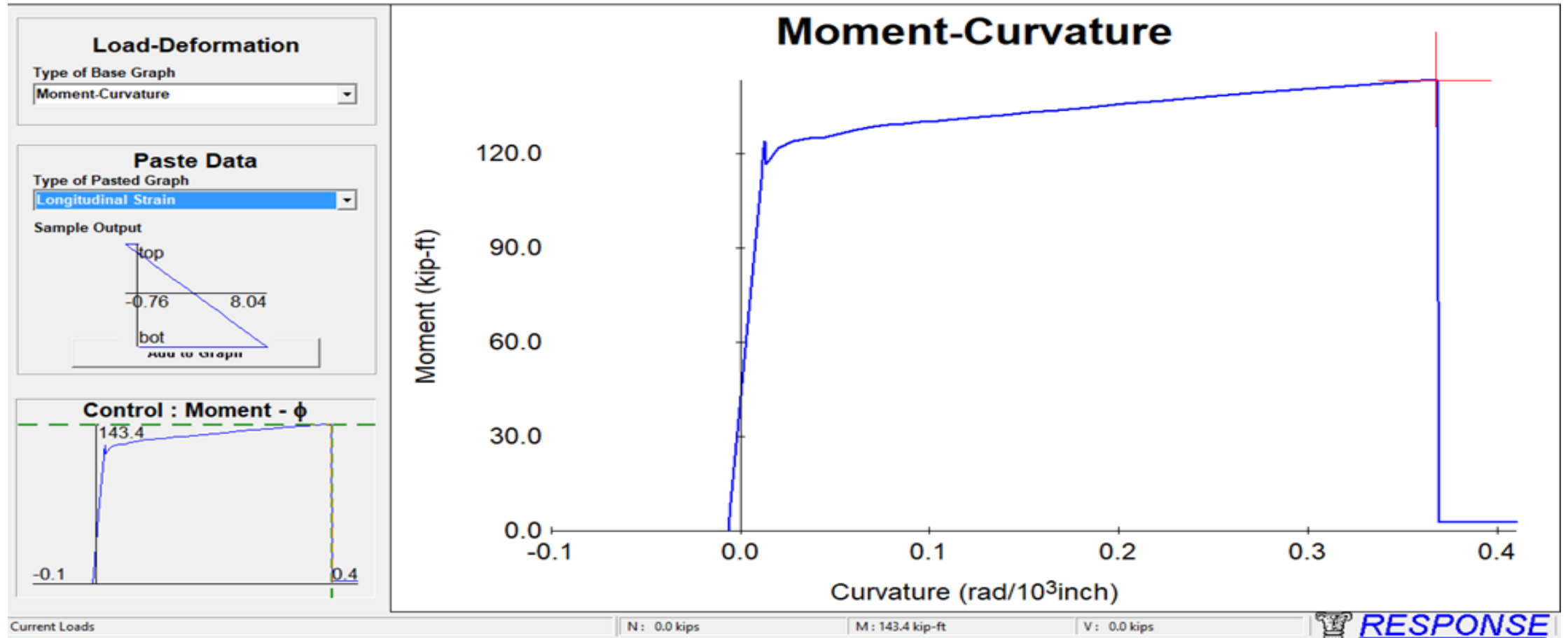


Figure 26. Response 2000 Output

## TASK 4.2: PREDICTION CALCULATIONS

- Deflection - .477 inches
- Camber - .042 inches

$$l(\Delta) = \int_0^l \frac{Mm}{EI} dx$$

$\Delta$  = Deflection (in)

$M$  = Internal Moments in the beam in the real diagram (kip\*in)

$m$  = Internal moments in the beam in the virtual diagram (kip\*in)

$E$  = Modulus of Elasticity (ksi)

$I$  = Effective moment of Inertia (in<sup>4</sup>)

$$\Delta_c = \frac{1}{8} * \frac{PeL^2}{Ee}$$

$\Delta_c$  = Deflection due to Camber (in)

$P$  = Prestressing force (kips)

$e$  = Eccentricity (in)

$L$  = Length of the beam (in)

$E$  = Modulus of Elasticity (ksi)

$I_e$  = Effective moment of Inertia (in<sup>4</sup>)



Figure 27. Beam Bending

# TASK 4.2: PREDICTION CALCULATIONS

## Losses

- **Elastic Shortening** = 3.38 ksi
  - Beam length gets shorter
- **Creep of Concrete** = 4.28 ksi
  - Pressure causes deformation in the concrete



Figure 28. Last year's formwork

# TASK 4.2: PREDICTION CALCULATIONS

## Losses

- **Shrinkage of Concrete** = 10.29 ksi
  - Drying of concrete affects stretch of the strands
  - Average annual humidity percentage
- **Relaxation of Tendons** = 4.28 ksi
  - Strands relaxation over time



Figure 29. Last year's Screeding of Concrete

# TASK 5: SHOP DRAWINGS

## 5.1 AutoCAD

- 5.1.1 Side Elevation
- 5.1.2 Cross Section
- 5.1.3 Profile View



Figure 30. AutoCAD Logo

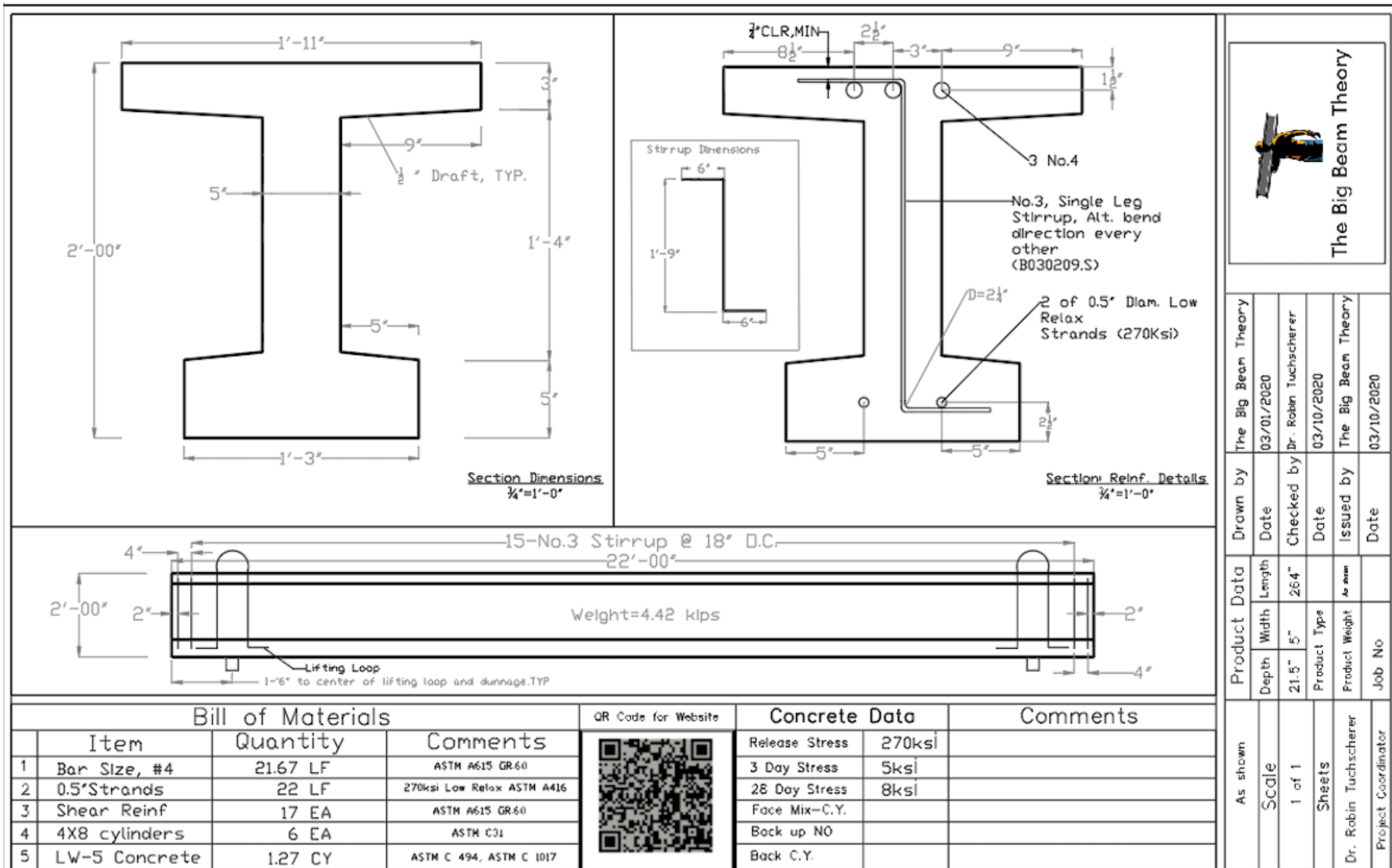


Figure 31. Shop Drawings

# TASK 5.1.1: SIDE ELEVATION

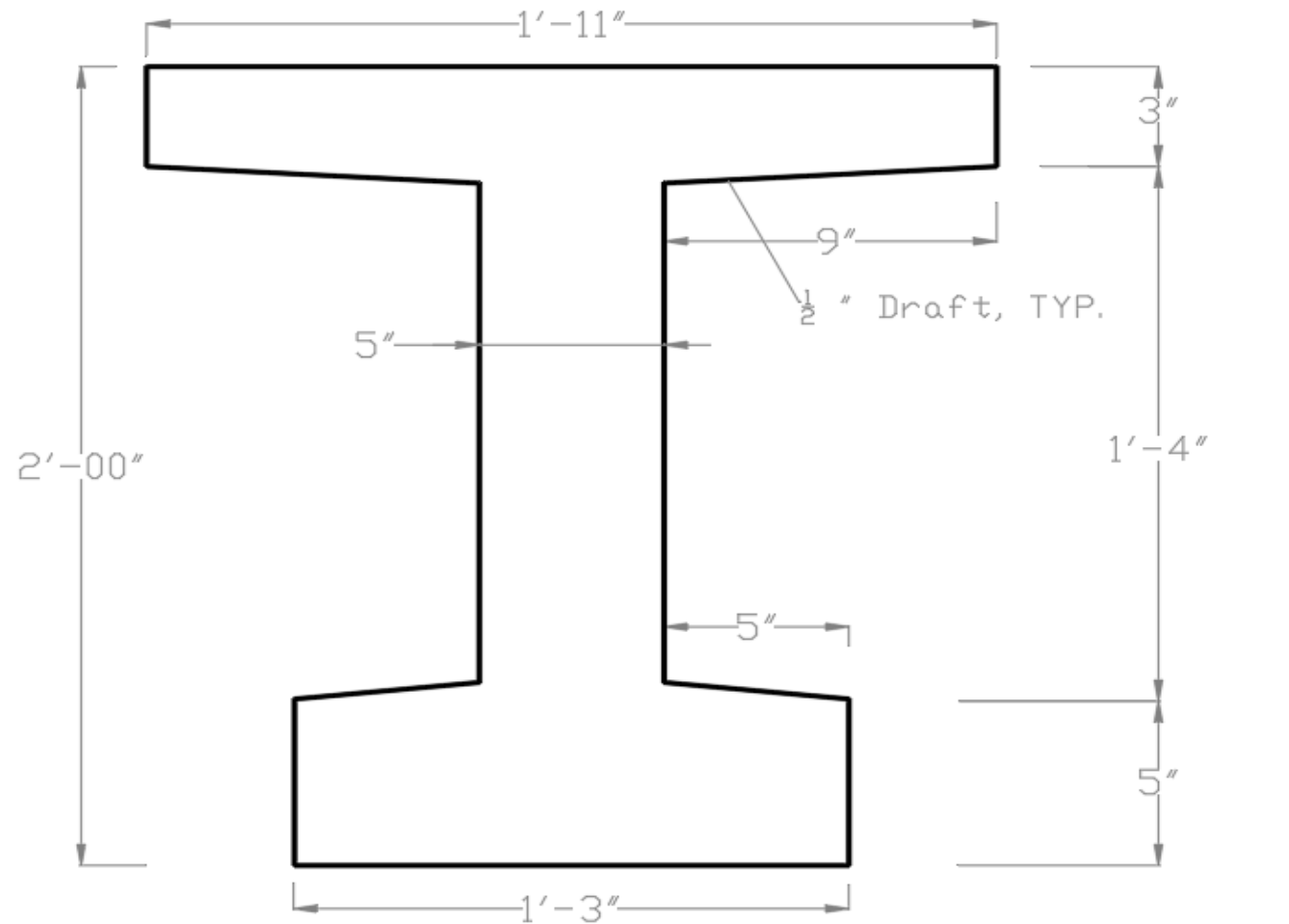
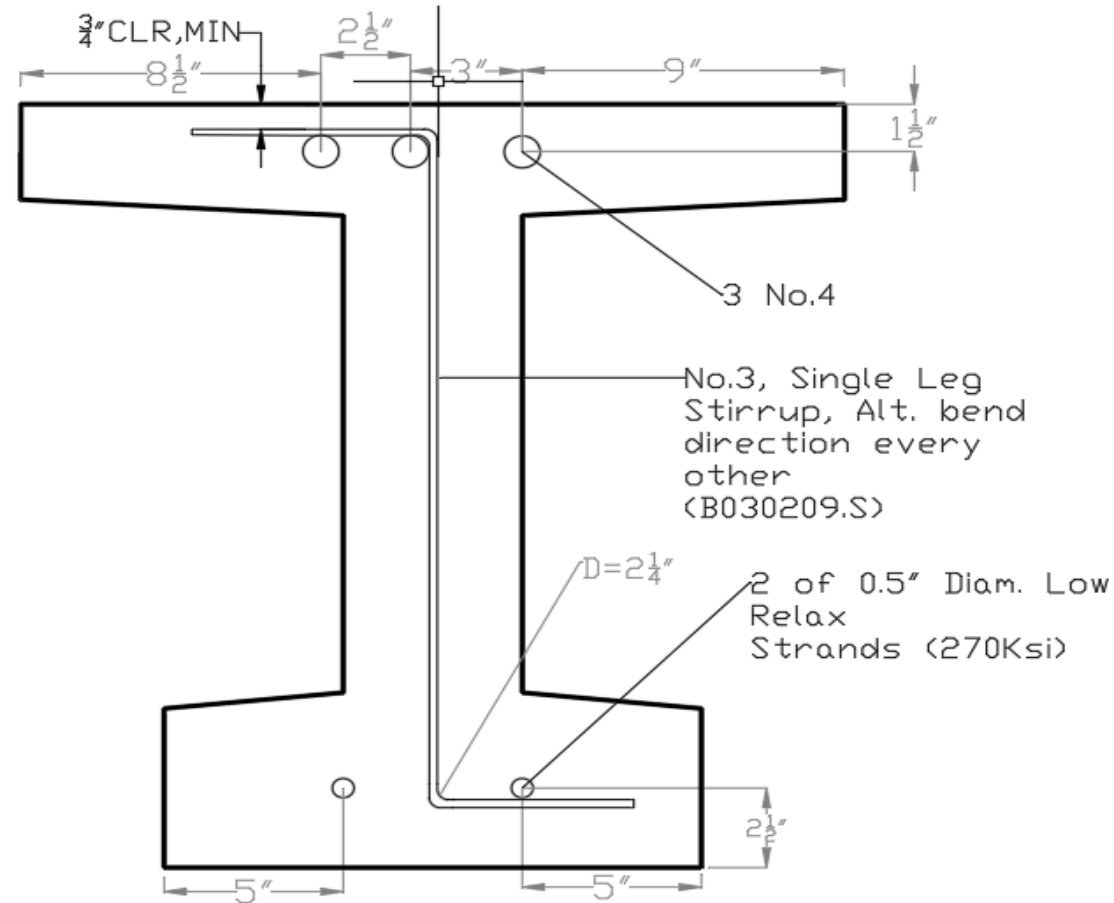


Figure 32. Side Elevation



# TASK 5.1.2: CROSS SECTION



Section: Reinf. Details  
3/4"=1'-0"

Figure 33. Cross Section

# TASK 5.1.3: PROFILE VIEW

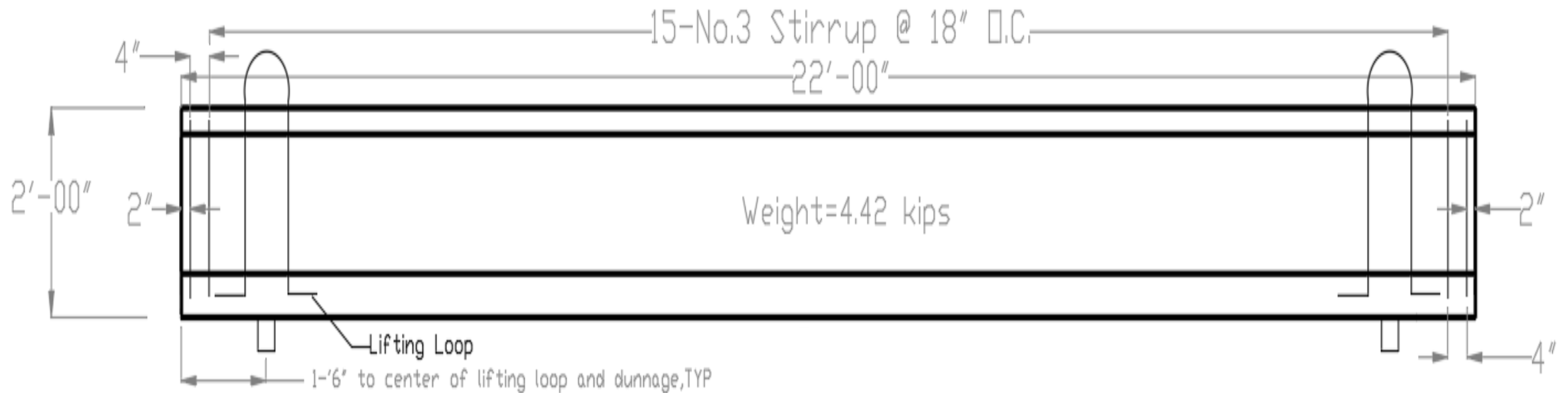


Figure 34. Profile View



Figure 35. Beam at TPAC facility

## TASK 6: CASTING OF BEAM

### Casting Info:

- Poured on 3/23 at 9am in Phoenix
- The Beam should be approaching 8,000 psi



Figure 36. Last Year's Beam at NAU Lab

## TASK 7: TESTING OF BEAM

Current Status of Beam:

- The beam is still at TPAC facility because of COVID-19
- The beam will be tested early May if the “stay at home” order is lifted



# TASK 8: PROJECT MANAGEMENT

Reports

Website

Meetings

- Team
- Grading Instructor
- Technical Advisor



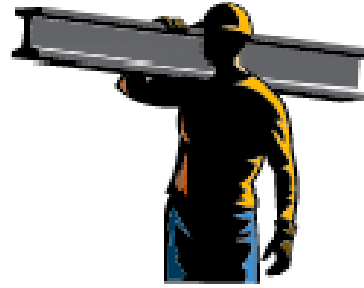
Figure 37. Team Website

## TASK 9: PROJECT IMPACTS

- Regulatory: Competition rules
- Environmental: Mining of cement is the 3<sup>rd</sup> largest CO<sub>2</sub> emissions in the world.
- Social: Winning can bring NAU more students by showing potential students that NAU can beat top ranked schools in competitions
- Economic: Increases the demand of jobs for getting the materials for the concrete and casting the beam

# WHAT WE WOULD DO DIFFERENT

- Build more float into schedule
- Weekly calendar updates
- More TA meetings
- Better communication with TPAC
- Start design earlier
- Stay on top of design work



# The Big Beam Theory

Figure 38. The Big Beam Theory Logo

ANY QUESTIONS?  
THANK YOU FOR LISTENING



# REFERENCES

- [1] R. Tuchscherer, *Lecture Slides*, Flagstaff: NAU, 2019.
- [2] "2019-2020 PCI Competition".
- [3] ACI 318-19 Code
- [4] PCI Design Handbook 7<sup>th</sup> Edition